

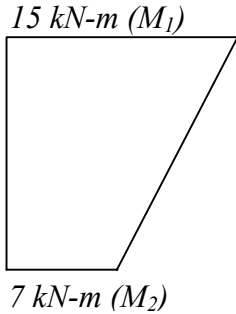
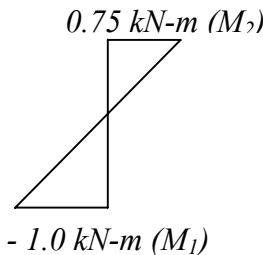
<h1>Structural Steel Design Project</h1> <h2>Calculation Sheet</h2>	Job No:	Sheet <i>1 of 6</i>	Rev																																												
	Job Title: <i>BEAM COLUMN</i>																																														
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<p><b>PROBLEM: 1</b></p> <p><i>A non – sway intermediate column in a building frame with flexible joints is 4.0 m high and it is ISHB 300 @ 588 N/m steel section. Check the adequacy of the section when the column is subjected to following load:</i></p> <p><i>Factored axial load = 500 kN</i></p> <p><i>Factored moments:</i></p> <table style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th></th> <th style="text-align: center;"><math>M_z</math></th> <th style="text-align: center;"><math>M_y</math></th> </tr> </thead> <tbody> <tr> <td style="text-align: right;"><i>Bottom</i></td> <td style="text-align: center;"><i>+ 7.0 kN – m</i></td> <td style="text-align: center;"><i>- 1.0 kN - m</i></td> </tr> <tr> <td style="text-align: right;"><i>Top</i></td> <td style="text-align: center;"><i>+ 15.0 kN – m</i></td> <td style="text-align: center;"><i>+ 0.75 kN - m</i></td> </tr> </tbody> </table> <p><i>[ <math>f_y = 250 \text{ N/mm}^2</math> ; <math>E = 2 * 10^5 \text{ N/mm}^2</math> ]</i></p> <p><i>Assume effective length of the column as 3.4 m along both the axes.</i></p> <p><b>CROSS-SECTION PROPERTIES:</b></p> <table style="margin-left: auto; margin-right: auto;"> <tbody> <tr> <td><i>Flange thickness</i></td> <td style="text-align: center;">=</td> <td><i>T</i></td> <td style="text-align: center;">=</td> <td><i>10.6 mm</i></td> </tr> <tr> <td><i>Clear depth between flanges</i></td> <td style="text-align: center;">=</td> <td><i>d</i></td> <td style="text-align: center;">=</td> <td><i>300 – (10.6 * 2)</i> <i>= 278.8 mm</i></td> </tr> <tr> <td><i>Thickness of web</i></td> <td style="text-align: center;">=</td> <td><i>t</i></td> <td style="text-align: center;">=</td> <td><i>7.6 mm</i></td> </tr> <tr> <td><i>Flange width</i></td> <td style="text-align: center;">=</td> <td><i>2b</i></td> <td style="text-align: center;">=</td> <td><i>250 mm</i></td> </tr> <tr> <td></td> <td></td> <td><i>b</i></td> <td style="text-align: center;">=</td> <td><i>125 mm</i></td> </tr> <tr> <td><i>Area of cross-section</i></td> <td style="text-align: center;">=</td> <td><i>A<sub>g</sub></i></td> <td style="text-align: center;">=</td> <td><i>7485 mm<sup>2</sup></i></td> </tr> <tr> <td><i>C/c distance between flanges</i></td> <td style="text-align: center;">=</td> <td><i>h<sub>f</sub></i></td> <td style="text-align: center;">=</td> <td><i>289.4 mm</i></td> </tr> </tbody> </table>					$M_z$	$M_y$	<i>Bottom</i>	<i>+ 7.0 kN – m</i>	<i>- 1.0 kN - m</i>	<i>Top</i>	<i>+ 15.0 kN – m</i>	<i>+ 0.75 kN - m</i>	<i>Flange thickness</i>	=	<i>T</i>	=	<i>10.6 mm</i>	<i>Clear depth between flanges</i>	=	<i>d</i>	=	<i>300 – (10.6 * 2)</i> <i>= 278.8 mm</i>	<i>Thickness of web</i>	=	<i>t</i>	=	<i>7.6 mm</i>	<i>Flange width</i>	=	<i>2b</i>	=	<i>250 mm</i>			<i>b</i>	=	<i>125 mm</i>	<i>Area of cross-section</i>	=	<i>A<sub>g</sub></i>	=	<i>7485 mm<sup>2</sup></i>	<i>C/c distance between flanges</i>	=	<i>h<sub>f</sub></i>	=	<i>289.4 mm</i>
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$R_z = 129.5 \text{ mm}$ $r_y = 54.1 \text{ mm}$ $I_z = 12545.2 * 10^4 \text{ mm}^4$ $I_y = 2193.6 * 10^4 \text{ mm}^4$ $Z_z = 836.3 * 10^3 \text{ mm}^3$ $Z_y = 175.5 * 10^3 \text{ mm}^3$ $Z_{pz} = 953.4 * 10^3 \text{ mm}^3$ $Z_{py} = 200.1 * 10^3 \text{ mm}^3$			
<p>(i) <b>Type of section:</b></p> $\frac{b}{T} = \frac{125}{10.6} = 11.8 > 10.5 \varepsilon \text{ \& } < 15.7 \varepsilon$ $\frac{d}{t} = \frac{278.8}{7.6} = 36.7 < 42 \varepsilon$ $\text{where } , \varepsilon = \sqrt{\frac{250}{f_y}} = \sqrt{\frac{250}{250}} = 1.0$ <p>Hence, cross- section is “SEMI-COMPACT” (Class 3)</p>			<p><i>Table 3.1 of IS: 800</i></p>

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<p>(ii) <i>Check for resistance of cross-section to the combined effects for yielding:</i></p> $f_{yd} = f_y/\gamma_a = 250/1.15$ $= 217.4 \text{ N/mm}^2$ $A_g = 7485 \text{ mm}^2$ $Z_z = 836.3 \times 10^3 \text{ mm}^3$ $Z_y = 175.5 \times 10^3 \text{ mm}^3$ $P = 500 \text{ kN}$ $M_z = 15 \text{ kN-m}$ $M_y = 1.0 \text{ kN-m}$ <p><i>The interaction equation is:</i></p> $\frac{P_c}{A_g f_{yd}} + \frac{M_z}{Z_z f_{yd}} + \frac{M_y}{Z_y f_{yd}} \leq 1$ $= \frac{500 \times 10^3}{7485 \times 217.4} + \frac{15 \times 10^6}{836.3 \times 10^3 \times 217.4} + \frac{1 \times 10^6}{175.5 \times 10^3 \times 217.4}$ $= 0.307 + 0.083 + 0.026 = 0.416 < 1.0$ <p><i>Hence, section is O.K. against combined effects</i></p>			

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<p>(iii) <b>Check for resistance of cross-section to the combined effects for buckling:</b></p> <p>(a) <b>Determination of <math>P_{dz}</math>, <math>P_{dy}</math> and <math>P_d</math> (Clause 7.1.2) -----</b></p> <p><math>KL_y = KL_z = 3.4m</math></p> $\lambda_z = \frac{KL_z}{r_z} = \frac{3400}{129.5} = 26.03, \lambda_y = \frac{KL_y}{r_y} = 54.1 = 62.8$ $\lambda_1 = \pi \cdot (E / f_y)^{1/2} = 88.857$ <p>Therefore, non-dimensional slenderness ratios</p> $\lambda_z = \frac{\lambda_z}{\lambda_1} = 0.296 \text{ and } \lambda_y = \frac{\lambda_y}{\lambda_1} = 0.706$ <p>Calculation of <math>\chi</math> :</p> <p>Imperfection factors: <math>\alpha_z = 0.21</math> ; <math>\alpha_y = 0.34</math></p> <p><math>\phi</math> - values:</p> $\phi = 0.5[1 + \alpha(\bar{\lambda} - 0.2) + \bar{\lambda}^2]$ $\phi_z = 0.5[1 + 0.21(0.296 - 0.2) + (0.296)^2] = 0.554$ $\phi_y = 0.5[1 + 0.34(0.706 - 0.2) + (0.706)^2] = 0.835$ <p><math>\chi</math> - values:</p> $\chi = \frac{1}{\phi + (\phi^2 - \bar{\lambda}^2)^{1/2}} \leq 1.0$ $\chi_z = 1/[0.554 + (0.554^2 - 0.296^2)^{1/2}] = 0.978$ $\chi_y = 1/[1.006 + (0.835^2 - 0.706^2)^{1/2}] = 0.780$			

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<p><i>Therefore,</i></p> $P_{dz} = 7485 \times 0.978 \times 250 / 1.10 \times 10^{-3} = 1663.7 \text{ kN}$ $P_{dy} = 7485 \times 0.78 \times 250 / 1.10 \times 10^{-3} = 1327.0 \text{ kN}$ <p><b>Therefore <math>P_d = P_{dy} = 1327.0 \text{ kN}</math></b></p> <p><b>(b) Determination of <math>M_{dz}</math></b></p> <p>Elastic Critical moment is given by</p> $M_{cr} = \frac{\pi^2 EI_y h_f}{2L_{LT}^2} \left[ 1 + \frac{1}{20} \left[ \frac{L_{LT} / r_y}{h_f / t_f} \right]^2 \right]^{0.5}$ $M_{cr} = \frac{\pi^2 \times 2E5x2193.6E4x289.4}{2x(3400)^2} \left[ 1 + \frac{1}{20} \left\{ \frac{3400/54.1}{289.4/10.6} \right\}^2 \right]^{0.5} = 6.319 \times 10^8 \text{ N-m}$ $\lambda_{LT} = \sqrt{Z_{ez} \cdot f_y / M_{cr}} = \sqrt{836.3E3x250 / 6.319E8} = 0.5856$ $\phi_{LT} = 0.5 \left[ 1 + \alpha_{LT} (\lambda_{LT} - 0.2) + \lambda_{LT}^2 \right] = 0.5 \left[ 1 + 0.21x(0.586 - 0.2) + 0.586^2 \right] = 0.71$ <p>[<math>\alpha_{LT} = 0.21</math>]</p> $\chi_{LT} = \left[ \frac{1}{\phi_{LT} + \left\{ \phi_{LT}^2 - \lambda_{LT}^2 \right\}^{0.5}} \right] = 0.90 \leq 1.0$ $f_{bd} = \chi_{LT} \cdot f_y / \gamma_m = 0.90 \times 250 / 1.1 = 204.55 \text{ MPa}$ $M_{dz} = Z_{ez} \cdot f_{bd} = 836.3 \times 10^3 \times 204.55 \times 10^{-6} = 179.42 \text{ kN-M}$ <p><b>(c) Determination of <math>M_{dy}</math> -----</b></p> $M_{dy} = Z_{ey} \cdot f_y / \gamma_m = 175.5 \times 10^3 \times 250 / 1.1 \times 10^{-6} = 39.9 \text{ kN-M}$			
			<p><b>IS: 800</b> (Clause 9.3.2.2 Clause 8.2.2)</p>

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<p><i>The interaction equations to be satisfied</i></p> $\frac{P}{P_{dy}} + k_y \frac{C_{my} M_y}{M_{dy}} + k_{LT} \frac{M_z}{M_{dz}} \leq 1.0$ $\frac{P}{P_{dz}} + 0.6 k_y \frac{C_{my} M_y}{M_{dy}} + k_z \frac{C_{mz} M_z}{M_{dz}} \leq 1.0$ <p><b>(d) Determination of <math>C_{my}</math> -----</b></p> $\psi_z = M_2 / M_1 = 7/15 = 0.467$ $C_{my} = 0.6 + 0.4 \psi \geq 0.4$ $C_{my} = 0.6 + 0.4 \times 0.467 = 0.7868 \geq 0.4$ <p><b>(e) Determination of <math>C_{mz}</math> -----</b></p> $\psi_y = 0.75 / (-1.0) = -0.75$ $C_{mz} = 0.6 + 0.4 \psi \geq 0.4$ $C_{mz} = 0.6 - 0.4 \times 0.75 = 0.30 \approx 0.4$ <p><b>(f) Determination of <math>C_{mLT}</math> -----</b></p> $\psi_z = M_2 / M_1 = 7/15 = 0.467$ $C_{mLT} = 0.6 + 0.4 \psi \geq 0.4$ $C_{mLT} = 0.6 + 0.4 \times 0.467 = 0.7868 \geq 0.4$			
<div style="display: flex; justify-content: space-around; align-items: center;"> <div style="text-align: center;">  <p>15 kN-m (<math>M_1</math>)</p> <p>7 kN-m (<math>M_2</math>)</p> </div> <div style="text-align: center;">  <p>0.75 kN-m (<math>M_2</math>)</p> <p>- 1.0 kN-m (<math>M_1</math>)</p> </div> </div>			

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<p><b>(g) Determination of <math>k_z</math>, <math>k_y</math> &amp; <math>k_{LT}</math>-----</b></p> $k_y = 1 + (\lambda_y - 0.2)n_y \leq 1 + 0.8 n_y$ $k_z = 1 + (\lambda_z - 0.2)n_z \leq 1 + 0.8 n_z$ $k_{LT} = 1 - \frac{0.1\lambda_{LT}n_y}{(C_{mLT} - 0.25)} \geq 1 - \frac{0.1n_y}{(C_{mLT} - 0.25)}$ $n_y = P / P_{dy} = 500 / 1327 = 0.377$ $n_z = P / P_{dz} = 500 / 1663.7 = 0.30$ $\lambda_z = \frac{\lambda_z}{\lambda_1} = 0.296 ; \lambda_y = \frac{\lambda_y}{\lambda_1} = 0.706 \text{ and } \lambda_{LT} = 0.5856$ <p>Therefore,</p> $k_y = 1 + (0.706 - 0.2) \times 0.377 = 1.19 [\leq 1.3016 = 1 + 0.8 n_y]$ $k_z = 1 + (0.296 - 0.2) \times 0.30 = 1.03 [\leq 1.24 = 1 + 0.8 n_y]$ $k_{LT} = 1 - \frac{0.1 \times 0.5856 \times 0.377}{(0.7868 - 0.25)} = 0.959 \geq [1 - \frac{0.1 \times 0.377}{(0.7868 - 0.25)} = 0.93]$ <p><b>(h) Interaction checks-----</b></p> <p><b><u>Check no 1</u></b></p> $\frac{P}{P_{dy}} + k_y \frac{C_{my} M_y}{M_{dy}} + k_{LT} \frac{M_z}{M_{dz}}$ $= \frac{500}{1327} + 1.19 \times \frac{0.7868 \times 1.0}{39.9} + 0.93 \times \frac{15}{179.42}$ $= \mathbf{0.3767 + 0.023 + 0.077 = 0.478 < 1.0}$			

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<p><b><u>Check no 2</u></b></p> $\frac{P}{P_{dz}} + 0.6k_y \frac{C_{my} M_y}{M_{dy}} + k_z \frac{C_{mz} M_z}{M_{dz}} \leq 1.0$ $= \frac{500}{1663.7} + 0.6 \times 1.19 \times \frac{0.7868 \times 1.0}{39.9} + 1.03 \times \frac{0.4 \times 15}{179.42}$ $= \mathbf{0.30 + 0.014 + 0.034 = 0.348 < 1.0}$			